1/1/1/1

Substituting U = Q/A and the hydraulic diameter into the friction coefficient equation and rearranging gives

$$H = fL \frac{Q^2}{8g} \frac{P_r}{A^3}$$

The hydraulic diameter concept is adequate provided that the  $P_r/A^3$  of the cross-section is not significantly greater than that of any other cross-section than can be drawn inside it.

By rounding the corners of the cross-sections in Fig. 5.7 it is possible to reduce  $P_r/A^3$  by only 1 per cent, so the hydraulic diameter concept is adequate. Cross-sections with small areas influenced by a disproportionate amount of perimeter, as in the cross-section of Fig. 5.8, have  $P_r/A^3$  ratios larger than that of another cross-section that can be fitted within their perimeters. In the case of the cross-section shown in Fig. 5.8, the minimum  $P_r/A^3$  would

Substituting  $U\!=\!Q/A$  and the hydraulic diameter into the friction coefficient equation and rearranging gives

$$H = fL \frac{Q^2 P_v}{8a A^3}$$

The hydraulic diameter concept is adequate provided that the  $P_s/A^3$  of the cross-section is not significantly greater than that of any other cross-section than can be drawn inside it.

By rounding the corners of the cross-sections in Fig. 5.7 it is possible to reduce  $P_r/A^3$  by only 1 per cent, so the hydraulic diameter concept is adequate. Cross-sections with small areas influenced by a disproportionate amount of perimeter, as in the cross-section of Fig. 5.8, have  $P_r/A^3$  ratios larger than that of another cross-section that can be fitted within their perimeters. In the case of the cross-section shown in Fig. 5.8, the minimum  $P_r/A^3$  would

TREX-130713.0046